

Focussing & the Diffraction Limit

Ray Optics

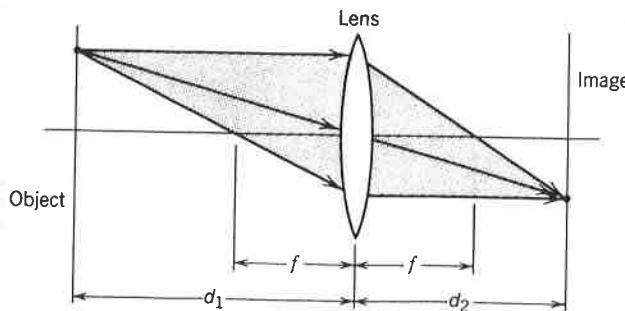


Figure 4.4-1 Rays in a focused imaging system.

↖ in focus when

$$\frac{1}{d_1} + \frac{1}{d_2} = \frac{1}{f}$$

~ define focussing error $\epsilon = \frac{1}{d_1} + \frac{1}{d_2} - \frac{1}{f}$

~ note, for object a long way away

$$d_1 \rightarrow \infty \Rightarrow d_2 = f$$

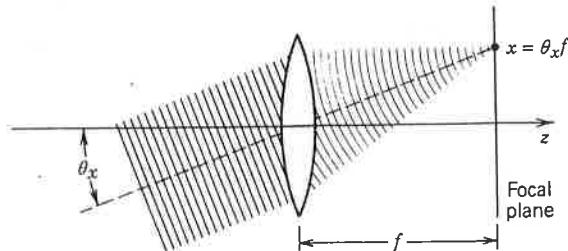


Figure 4.2-2 Focusing of a plane wave into a point. A direction (θ_x, θ_y) is mapped into a point $(x, y) = (\theta_x f, \theta_y f)$.

Wave Optics

~ off axis rays
focussed at different points

(7)

~ position at the focal plane

$$x_L = 0, f = \frac{2L_0}{d_1} f = \frac{k_m}{K}$$

~ lets look at an imaging system
with one lens

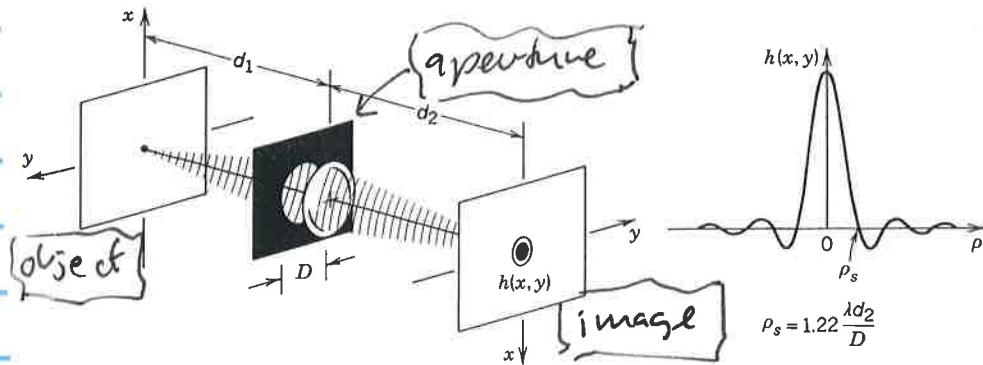
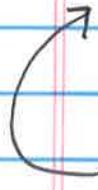


Figure 4.4-8 Impulse-response function of an imaging system with a circular aperture.



point on the object plane produces
a spherical wave

@ the aperture we have

$$u(x, y) = h_i e^{-ik(x^2+y^2)/2d_1}$$

Fresnel approximation

$$h_i = i \cancel{\lambda d_1} e^{-ikd_1}$$

(3)

~ just after the aperture

$$u(x, y) = h_1 e^{-ik(x^2 + y^2)/2d_1} p(x, y)$$

function that describes the aperture

~ this field is multiplied by the transfer function of the lens

$$u(x, y) = h_1 e^{-ik \frac{x^2 + y^2}{2d_1}} p(x, y) e^{ik \frac{x^2 + y^2}{2f}}$$

~ the field then propagates to the image plane at d_2

~ find the field at the image plane by convoluting $u(x, y)$ w/ the free space impulse-response function

$$h(x, y) = h_1 h_2 \iint e^{-ik \frac{x'^2 + y'^2}{2d_1}} p(x', y') e^{ik \frac{x'^2 + y'^2}{2f}} \times e^{-ik \frac{\pi}{\lambda d_2} ((x-x')^2 + (y-y')^2)} dx' dy'$$

$$h_2 = \frac{i}{\lambda d_2} e^{-ik d_2}$$

(4)

~ we can now use the Fraunhofer

approximation \leftarrow ignore x^2, y^2 terms
in the exponentials
($x^2, y^2 \ll \lambda d$)

$$h(x, y) = h_1 h_2 \iint e^{-ik \frac{c}{2} (\frac{1}{d_1} + \frac{1}{d_2} - \frac{1}{f}) (x'^2 + y'^2)} \times p(x', y') \\ \times e^{i2\pi (\frac{v_x}{\lambda d_2} x' + \frac{v_y}{\lambda d_2} y')} dx' dy'$$

$$= h_1 h_2 \iint e^{-ik \frac{c}{2} (x'^2 + y'^2)} p(x', y') \\ e^{i2\pi (v_x x' + v_y y')} dx' dy'$$

where $v_x = \frac{v_x}{\lambda d_2}$, $v_y = \frac{v_y}{\lambda d_2}$ ~ as before
w/ diff. $\frac{v}{\lambda d}$

and $c = \frac{1}{d_1} + \frac{1}{d_2} - \frac{1}{f}$ \hookrightarrow focassing error

~ when the system is "in focus"

$$\frac{1}{d_1} + \frac{1}{d_2} = \frac{1}{f} \Rightarrow c = 0$$

(5)

$$\Rightarrow h(x, y) = h_1 h_2 \iint p(x', y') e^{i2\pi(v_x x' + v_y y')} dx' dy'$$

Field at the image plane
is the F.T. of the aperture
function $p(x, y)$

$$\text{write as: } h(x, y) = h_1 h_2 P\left(\frac{x}{\lambda d_2}, \frac{y}{\lambda d_2}\right)$$

This is the same
as the diffraction
problem.

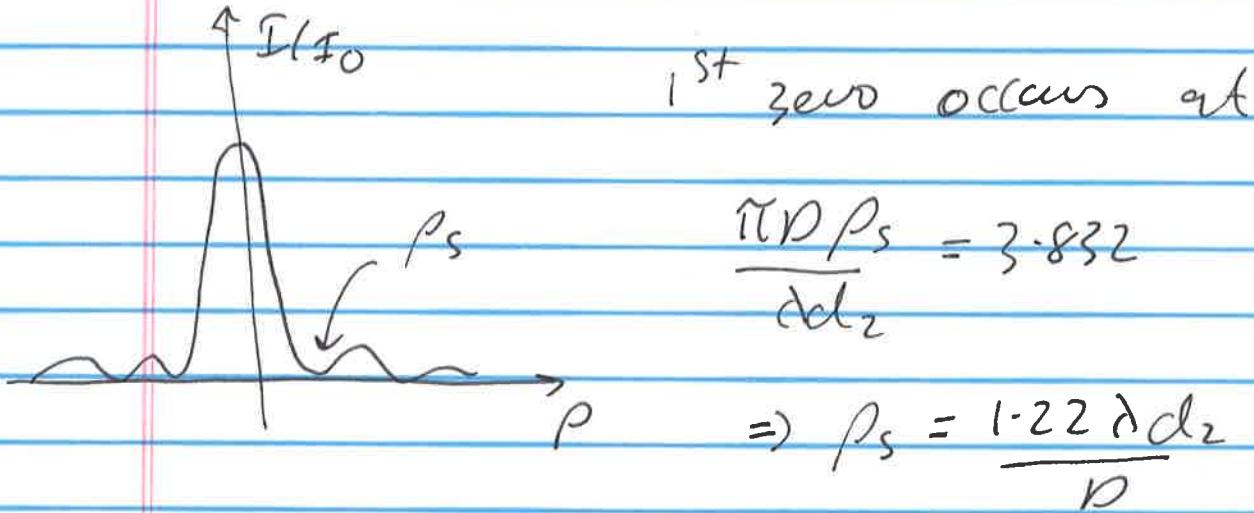
for circular aperture

$$h(x, y) = h_1 h_2 \frac{D}{2} \frac{\mathcal{J}_1(\hat{\pi} D p(\lambda d))}{p(\lambda d)}$$

\Rightarrow pt. spot at the object plane appears
as an "Airy disk" at the image plane

~ characterize size by the radius
where the Airy disk has its 1st zero

(6)

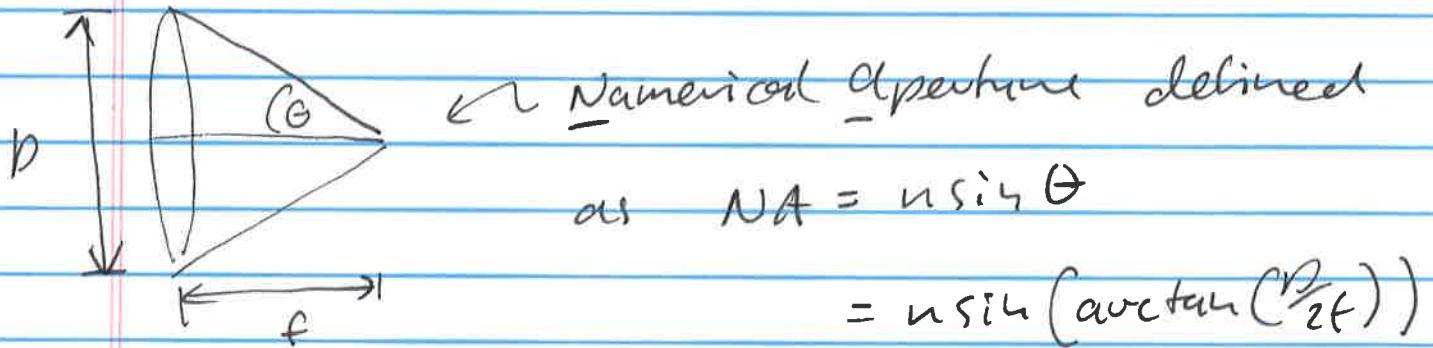


~if the object plane is far away ($d_o \rightarrow \infty$)

then $d_2 \approx f$

$$\Rightarrow \rho_s \approx \frac{1.22 \lambda f}{D} = 1.22 \lambda F_{\#} \leftarrow \begin{array}{l} \text{F-number} \\ \text{of the lens} \end{array}$$

$$F_{\#} = f/D$$



$$\approx \frac{nD}{2f} = \frac{n}{2} F_{\#}$$

(7)

$$\Rightarrow NA = \frac{1}{2} F_{\#} \text{ for air } (n=1)$$

$$\Rightarrow \text{critical radius } \rho_s = \frac{1.22\lambda}{2NA} = \frac{\lambda}{1.6NA}$$

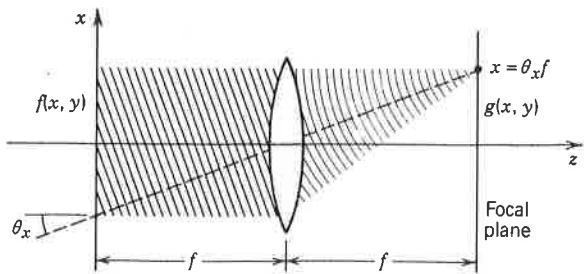
This is the "diffraction limit"

Note ~ The "diffraction limit" comes from diffraction through the optical system i.e. it is from the limited NA of the lens

~ high spatial resolution is achieved by collecting light over a large angle \hookrightarrow high spatial frequencies and \therefore fine distance resolution

$$v_{sc} \approx \theta_{sc}/\lambda$$

- our ability to resolve 2 objects, in either a telescope or a microscope, is determined by the diffraction limit
- ~ for example, imaging waves originating from 2 pts at the object plane at $\lambda l = 0$ and $\lambda l = \lambda l_0$
- ~ waves are focused at different points on the image plane according to the angle that the waves make with the lens



$$Q_x = \frac{\lambda l_0}{d_1}$$

Figure 4.2-4 Fourier transform system. The Fourier component of $f(x, y)$ with spatial frequencies ν_x and ν_y generates a plane wave at angles $\theta_x = \lambda\nu_x$ and $\theta_y = \lambda\nu_y$ and is focused by the lens to the point $(x, y) = (f\theta_x, f\theta_y) = (\lambda f\nu_x, \lambda f\nu_y)$ so that $g(x, y)$ is proportional to the Fourier transform $F(x/\lambda f, y/\lambda f)$.

~ let's be more rigorous

(9)

~ for the pt. @ (x_0, y_0) in the object plane, light has the form

$$ik((x-x_0)^2 + (y-y_0)^2)/2d,$$

$$U(x, y) = h_1 e$$

~ following the same steps as we did at the start of the lecture we get

$$U(x, y) = h_1 h_2 \iint e^{-ik((x-x_0)^2 + (y-y_0)^2)/2d} \times \rho(x', y') e^{ik(x'^2 + y'^2)/2f} \times e^{-ik((x-x')^2 + (y-y')^2)/2d_2} dx' dy'$$

if we ignore the x^2, y^2, x_0^2, y_0^2 terms
(Fresnel approximation)

$$U(x, y) = h_1 h_2 \iint e^{-ik/2(d_1 + d_2 - f)} (x'^2 + y'^2) \times \rho(x', y') \times e^{i2\pi(\frac{x_0}{\lambda d_1} x' + \frac{y_0}{\lambda d_1} y' + \frac{x}{\lambda d_2} x' + \frac{y}{\lambda d_2} y')} dx' dy'$$

↗

again, assume we are

$$\text{in focus} \Rightarrow f = \frac{1}{d_1} + \frac{1}{d_2} - \frac{1}{f} = 0$$

(10)

$$\Rightarrow h(x, y) = h_1 h_2 \iint p(x', y') e^{j2\pi \left[\left(\frac{x_o}{\lambda d_1} + \frac{x}{\lambda d_2} \right) x' + \left(\frac{y_o}{\lambda d_1} + \frac{y}{\lambda d_2} \right) y' \right]} dx' dy'$$

$$= h_1 h_2 P \left[\frac{x_o}{\lambda d_1} + \frac{x}{\lambda d_2}, \frac{y_o}{\lambda d_1} + \frac{y}{\lambda d_2} \right]$$

↗

F.T. of $P(x, y)$ evaluated

$$\text{at } v_x = \frac{x_o}{\lambda d_1} + \frac{x}{\lambda d_2}; v_y = \frac{y_o}{\lambda d_1} + \frac{y}{\lambda d_2}$$

$$\text{write } v_x = \frac{1}{\lambda d_2} \left(x + \frac{d_2}{d_1} x_o \right)$$

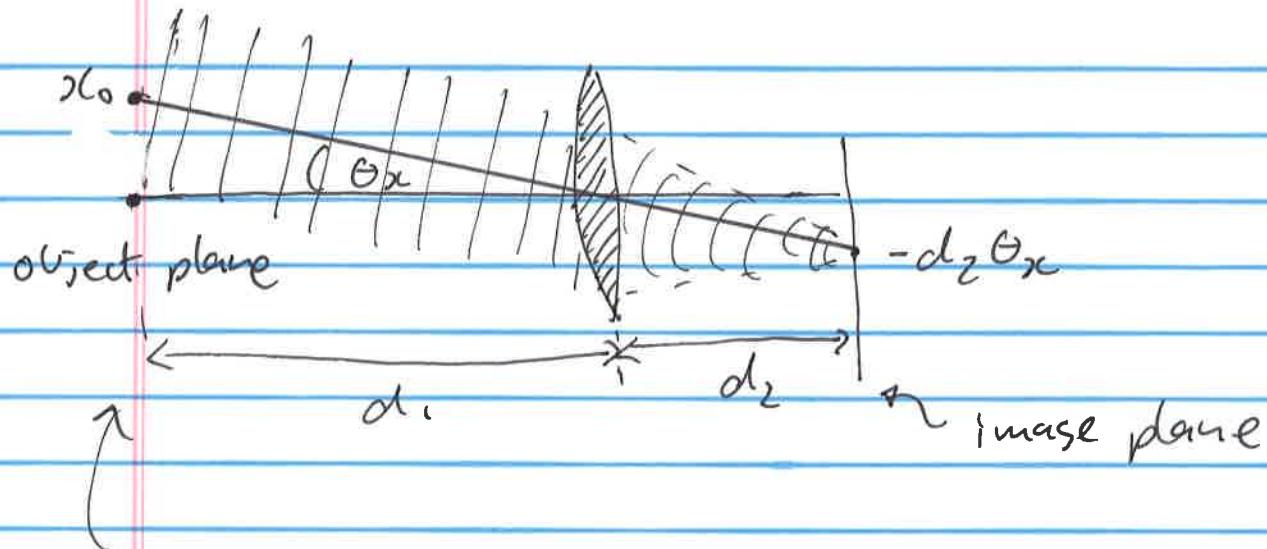
$$= \frac{1}{\lambda d_2} (x + d_2 \theta_x)$$

$$\text{likewise } v_y = \frac{1}{\lambda d_2} (y + d_2 \theta_y)$$

\Rightarrow pt at (x_o, y_o) in the object plane

produces an tiny disk at

$(x, y) = (-d_2 \theta_x, -d_2 \theta_y)$ in the image plane



whether light from an object at (x_0, y_0) can be resolved from light from an object at $(0,0)$ depends on the size of the Airy disk

Example (resolution for a telescope)

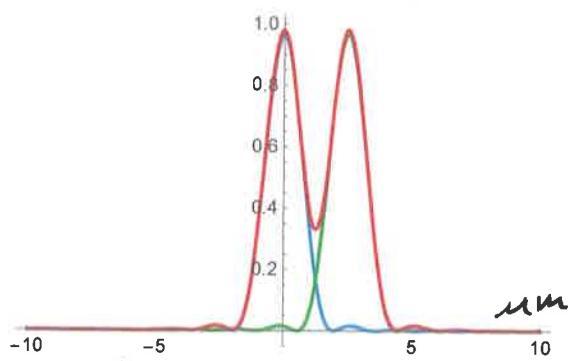
1" Ø lens at 2" focal length.

$$\Rightarrow \text{NA} = 0.25 \quad f \approx 50 \text{ mm} = 5 \times 10^4 \text{ nm}$$

assume $\lambda = 0.8 \text{ nm}$

$$\text{plot } I = \left(\frac{\int_1 (\pi D_p / \lambda d_2)}{\rho} \right)^2 = \left(\frac{\int_1 (2\pi \text{NA} p / \lambda)}{\rho} \right)^2$$

(12)



$$\Theta_y = 0$$

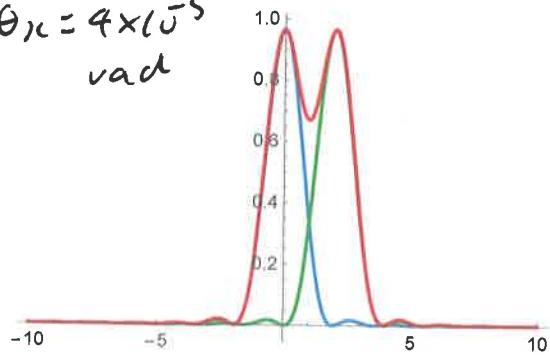
$$\theta_{\text{rc}} = 5 \times 10^{-5} \text{ rad}$$

\sim peak @

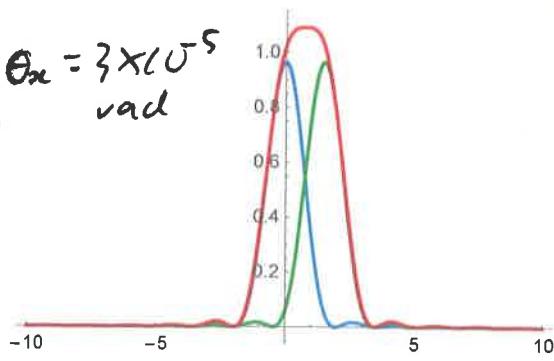
$$\lambda = f \theta_{\text{rc}} = 2.5 \text{ mm.}$$

\sim assume $d_i = 1 \text{ km} \Rightarrow \lambda_0 = d_i \theta_{\text{rc}} = 5 \text{ cm}$

$$\theta_{\text{rc}} = 4 \times 10^{-5} \text{ rad}$$



$$\theta_{\text{rc}} = 3 \times 10^{-5} \text{ rad}$$



$$\lambda_0 = 4 \text{ cm}$$

\Rightarrow just resolved

$$\lambda_0 = 3 \text{ cm}$$

\sim not resolved

Rayleigh Criterion: resolve 2 objects when
the center of the Airy
disk of one occurs at the 1st zero of the other

1st zero occurs when $\frac{2\pi NA \lambda}{\lambda} = 3.832$

$$\Rightarrow x_c = \frac{0.61\lambda}{NA}$$

$$\Theta_n = \frac{x_c}{f} = \frac{x_0}{d_i} \Rightarrow x_0 = \frac{0.61\lambda}{NA} \times \frac{d_i}{f}$$

= 3.9 cm for
our example

Microscope: more productive to think of
resolution in terms of the
spot size

Airy disk: spot size = $\frac{2 \times 0.61\lambda}{NA} = \frac{1.22\lambda}{NA}$

Gaussian beam: spot size = $2w_0 = \frac{2\lambda}{\pi NA} = \frac{0.64\lambda}{NA}$