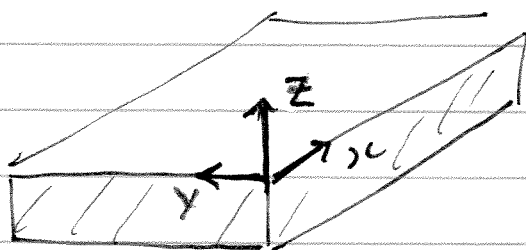


(1)

Optics & SpectroscopyLecture (7)

~ EM waves at metal-dielectric interfaces

System:



~ assume wave travels in the x-direction

$$\vec{E} = \vec{E}_0 e^{i(kx - \omega t)}$$

Maxwell's Equations $\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$

$$\nabla \times \vec{H} = \frac{\partial \vec{D}}{\partial t}$$

where $\vec{D} = \epsilon_0 \vec{E} + \vec{P}$ $\leftarrow \vec{P} = \epsilon_0 \chi \vec{E}$
 $\vec{B} = \mu_0 \vec{H}$
 $\Rightarrow \vec{D} = \epsilon_0 \epsilon_r \vec{E}$

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and the dielectric constant (rel. permittivity) is defined as: $\epsilon_r = (1 + \chi)$

for "harmonic" waves: $\frac{\partial \vec{E}}{\partial t} = -i\omega \vec{E}$

$$+ \frac{\partial \vec{H}}{\partial t} = -i\omega \vec{H}$$

$$\Rightarrow \nabla \times \vec{E} = i\omega \mu_0 \vec{H} \quad - (1)$$

$$+ \nabla \times \vec{H} = -i\omega \epsilon_0 \epsilon_r \vec{E} \quad - (2)$$

From (1): $\nabla \times \vec{E} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ E_x & E_y & E_z \end{vmatrix}$

x-component: $\frac{\partial E_z}{\partial y} - \frac{\partial E_y}{\partial z} = i\omega \mu_0 H_x$

y-component: $-\left(\frac{\partial E_z}{\partial x} - \frac{\partial E_x}{\partial z}\right) = i\omega \mu_0 H_y$

z-component: $\frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y} = i\omega \mu_0 H_z$

From (2):

$$x\text{-component: } \frac{\partial H_z}{\partial y} - \frac{\partial H_y}{\partial z} = -i\omega_0 \epsilon_0 \epsilon_r E_x$$

$$y\text{-component: } -\left(\frac{\partial H_z}{\partial x} - \frac{\partial H_x}{\partial z}\right) = -i\omega \epsilon_0 \epsilon_r E_y$$

$$z\text{-component: } \frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} = -i\omega \epsilon_0 \epsilon_r E_z$$

Note: wave is "homogeneous" in

the y -direction & propagates along x

$$\Rightarrow \frac{\partial E}{\partial y} = 0 \quad + \quad \frac{\partial E}{\partial x} = ikE$$

$\Rightarrow$ Equations for H_i become:

$$-\frac{\partial E_y}{\partial z} = i\omega\mu_0 H_x$$

$$-ikE_z + \frac{\partial E_x}{\partial z} = i\omega\mu_0 H_y$$

$$ikE_y = i\omega\mu_0 H_z$$

Likewise, equations for E_i become:

$$-\frac{\partial H_y}{\partial z} = -i\omega \epsilon_0 \epsilon_r E_x$$

$$-ik H_z + \frac{\partial H_x}{\partial z} = -i\omega \epsilon_0 \epsilon_r E_y$$

$$ik H_y = -i\omega \epsilon_0 \epsilon_r E_z$$

Two types of modes to consider:

TM = "transverse magnetic"

TE = "transverse electric"

~ look @ TM modes first

$$\text{have } H_y \neq 0 \Rightarrow E_y = 0$$

$$\Rightarrow H_x = H_z = 0$$

i.e. only E_x , E_z , H_y are non-zero

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$\Rightarrow$ left w/ three equations:

$$\frac{\partial E_x}{\partial z} - i k E_z = i \omega \mu_0 H_y \quad - (1)$$

$$-\frac{\partial H_y}{\partial z} = -i \omega \epsilon_0 \epsilon_r E_x \quad - (2)$$

$$i k H_y = -i \omega \epsilon_0 \epsilon_r E_z \quad - (3)$$

$\sim$ rewrite (2) & (3)

$$E_x = \frac{-i}{\omega \epsilon_0 \epsilon_r} \frac{\partial H_y}{\partial z} ; \quad E_z = \frac{-k}{\omega \epsilon_0 \epsilon_r} H_y$$

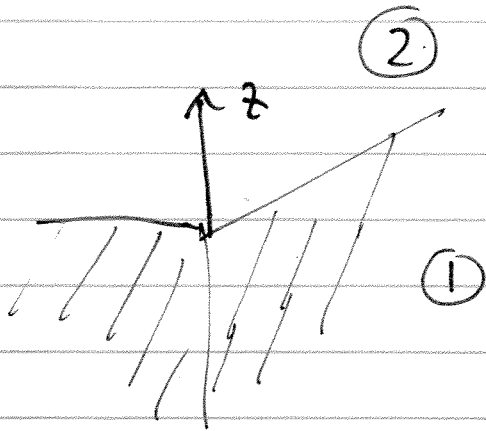
$\sim$ substitute into (1)

$$\frac{-i}{\omega \epsilon_0 \epsilon_r} \frac{\partial^2 H_y}{\partial z^2} + \frac{i k^2}{\omega \epsilon_0 \epsilon_r} H_y = i \omega \mu_0 H_y$$

$$\Rightarrow -\frac{\partial^2 H_y}{\partial z^2} = \{ \omega^2 \mu_0 \epsilon_0 \epsilon_r - k^2 \} H_y$$

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~ rewrite as
$$-\frac{\partial^2 H_y}{\partial z^2} = \left\{ \frac{\omega^2 \epsilon_0}{c_0^2} - k^2 \right\} H_y$$



medium (2) ~ dielectric

$$\Rightarrow \epsilon_2 \sim \text{real}$$

medium (1) ~ metal

$$\Rightarrow \epsilon_1 \sim \text{complex}$$

$$+ \text{Re}(\epsilon_1) < 0$$

~ interested in waves that are
confined to the interface

$$\Rightarrow \text{decay as: } \begin{aligned} &e^{-z/\delta_2} & z > 0 \\ &e^{z/\delta_1} & z < 0 \end{aligned}$$

$$\Rightarrow z > 0 \quad H_y(2) = A_2 e^{ikx} e^{-z/\delta_2} \quad - (1)$$

$$z < 0 \quad H_y(1) = A_1 e^{ikx} e^{z/\delta_1} \quad - (2)$$

(7)

From (1):

$$E_x = \frac{-i}{\omega \epsilon_0 \epsilon_r} \frac{\partial H_y}{\partial z} = \frac{-i}{\omega \epsilon_0 \epsilon_2} \left(\frac{-A_2}{\delta_2} \right) e^{ikx} e^{-z/\delta_2}$$

$$E_z = \frac{-k}{\omega \epsilon_0 \epsilon_r} H_y = \frac{-k A_2}{\omega \epsilon_0 \epsilon_2} e^{ikx} e^{-z/\delta_2}$$

Likewise, from (2):

$$E_x = \frac{-i}{\omega \epsilon_0 \epsilon_1} \left(\frac{A_1}{\delta_1} \right) e^{ikx} e^{+z/\delta_1}$$

$$E_z = \frac{-k A_1}{\omega \epsilon_0 \epsilon_1} e^{ikx} e^{+z/\delta_1}$$

~ tangential components of E & H have to be equal at the interface

$$\Rightarrow H_y(1) = H_y(2) \quad \text{at } z=0$$

$$\text{+ } E_x(1) = E_x(2) \quad \text{at } z=0$$

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from b.c. for H_y : $A_1 = A_2$

& from the b.c. for E_x :

$$\frac{i}{\omega \epsilon_0 \epsilon_2} \left(\frac{A_2}{\delta_2} \right) = \frac{-i}{\omega \epsilon_0 \epsilon_1} \left(\frac{A_1}{\delta_1} \right)$$

$$\Rightarrow \frac{\delta_1}{\delta_2} = - \frac{\epsilon_2}{\epsilon_1}$$

② = dielectric $\Rightarrow \epsilon_2 > 0$

$\therefore$ This means that ϵ_1 must be < 0

for a guided wave (so, ① must be a metal!)

Back to our wave equation:

$$-\frac{\partial^2 H_y}{\partial z^2} = \left\{ \frac{\omega^2 \epsilon_0}{c_0^2} - k^2 \right\} H_y$$

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now $\frac{\partial^2 \mathcal{H}_4}{\partial z^2} = \frac{1}{\delta z^2}$

$$\Rightarrow \frac{1}{\delta z^2} = - \left(\frac{\omega^2 \epsilon_2}{c_0^2} - k^2 \right)$$

$$\& \frac{1}{\delta z^2} = - \left(\frac{\omega^2 \epsilon_1}{c_0^2} - k^2 \right)$$

$$\frac{\delta z^2}{\delta z^2} = \frac{\epsilon_2^2}{\epsilon_1^2} = \frac{\left(\frac{\omega^2 \epsilon_2}{c_0^2} - k^2 \right)}{\left(\frac{\omega^2 \epsilon_1}{c_0^2} - k^2 \right)}$$

~ rearrange:

$$\frac{1}{\epsilon_1^2} \left(\frac{\omega^2 \epsilon_1}{c_0^2} - k^2 \right) = \frac{1}{\epsilon_2^2} \left(\frac{\omega^2 \epsilon_2}{c_0^2} - k^2 \right)$$

$$\left(\frac{\omega^2}{c_0^2 \epsilon_1} - \frac{k^2}{\epsilon_1^2} \right) = \left(\frac{\omega^2}{c_0^2 \epsilon_2} - \frac{k^2}{\epsilon_2^2} \right)$$

$$\frac{\omega^2}{c_0^2} \left(\frac{1}{\epsilon_1} - \frac{1}{\epsilon_2} \right) = k^2 \left(\frac{1}{\epsilon_1^2} - \frac{1}{\epsilon_2^2} \right)$$

seek an
expression
that
links ω
& k

$$\frac{\omega}{c_0} \sqrt{\frac{\epsilon_L - \epsilon_1}{\epsilon_1 \epsilon_L}} = k \sqrt{\frac{\epsilon_L^2 - \epsilon_1^2}{\epsilon_1^2 \epsilon_L^2}}$$

$$\Rightarrow k = \frac{\omega}{c_0} \sqrt{\frac{\epsilon_L - \epsilon_1}{\epsilon_L^2 - \epsilon_1^2}} \times \sqrt{\epsilon_1 \epsilon_L}$$

$$\boxed{k = \frac{\omega}{c_0} \sqrt{\frac{\epsilon_1 \epsilon_L}{\epsilon_1 + \epsilon_L}}} \leftarrow \text{desired result}$$

~ This is a "dispersion" relation

that shows how k changes w/ ω

~ not a linear relationship b/c

ϵ_i is a function of ω

clt light: $k = n \frac{\omega}{c_0}$

↖
linear dispersion relation

(11)

Use Drude model for metal

$$\epsilon_1 = \epsilon_{1r} + i\epsilon_{1i}$$

$$\epsilon_{1r} = 1 - \frac{\omega_p^2}{\omega^2} \quad \& \quad \epsilon_{1i} = \frac{\omega_p^2}{\omega^3} \tau$$

$\sim$ for optical frequencies $\epsilon_{1r} \gg \epsilon_{1i}$

$$\Rightarrow k \simeq \frac{\omega}{c_0} \sqrt{\frac{\epsilon_2(1 - \omega_p^2/\omega^2)}{1 + \epsilon_2 - \omega_p^2/\omega^2}}$$

Look at limits: large k ($k \rightarrow \infty$)

$$1 + \epsilon_2 - \frac{\omega_p^2}{\omega^2} \rightarrow 0$$

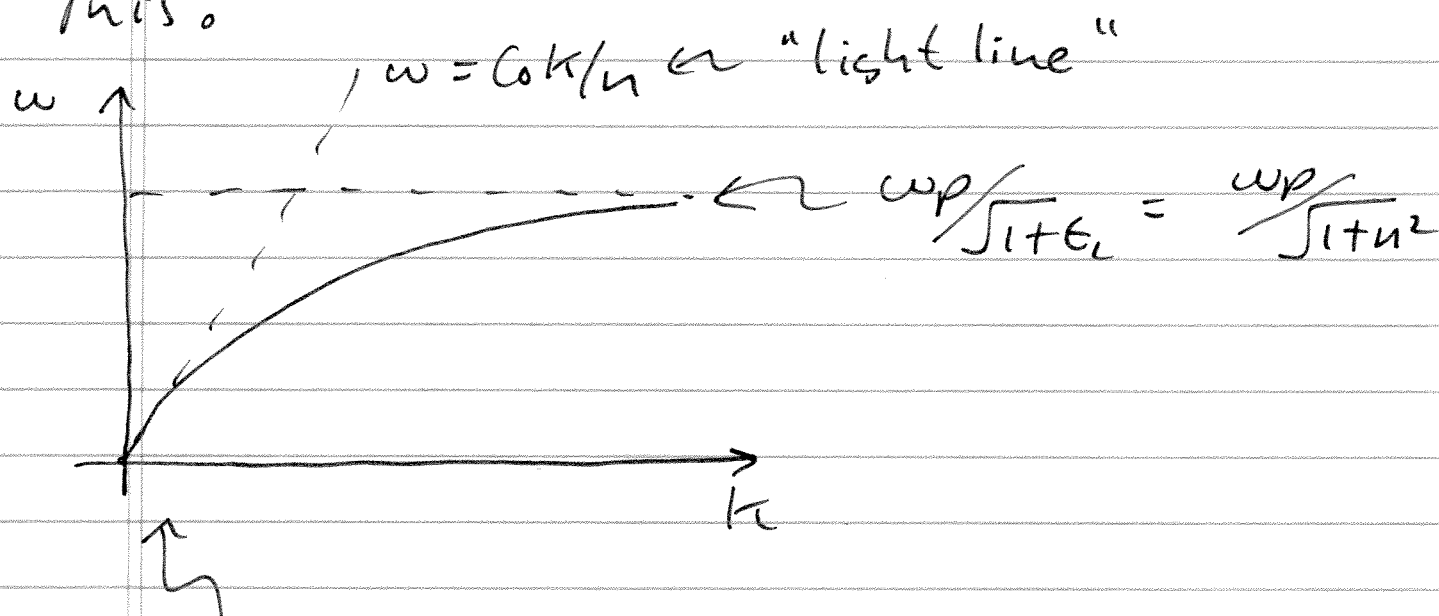
$$\Rightarrow \omega = \omega_p / \sqrt{1 + \epsilon_2}$$

$\sim$ small k ($k, \omega \rightarrow 0$)

$$k = \frac{\omega}{c_0} \sqrt{\frac{\epsilon_2(1 - \omega_p^2/\omega^2)}{1 + \epsilon_2 - \omega_p^2/\omega^2}} \simeq \frac{\omega \sqrt{\epsilon_2}}{c_0}$$

$$\frac{\omega \sqrt{\epsilon_2}}{c_0} = \frac{\omega n}{c_0} \sim \text{"light line"}$$

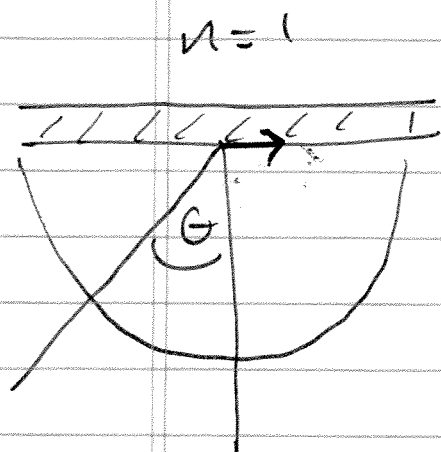
~ so the dispersion curve for "surface plasmons" (EM waves trapped at metal dielectric interfaces) looks like this:



wavevectors for SP & light don't meet $\Rightarrow$ can't excite SPs directly by photons

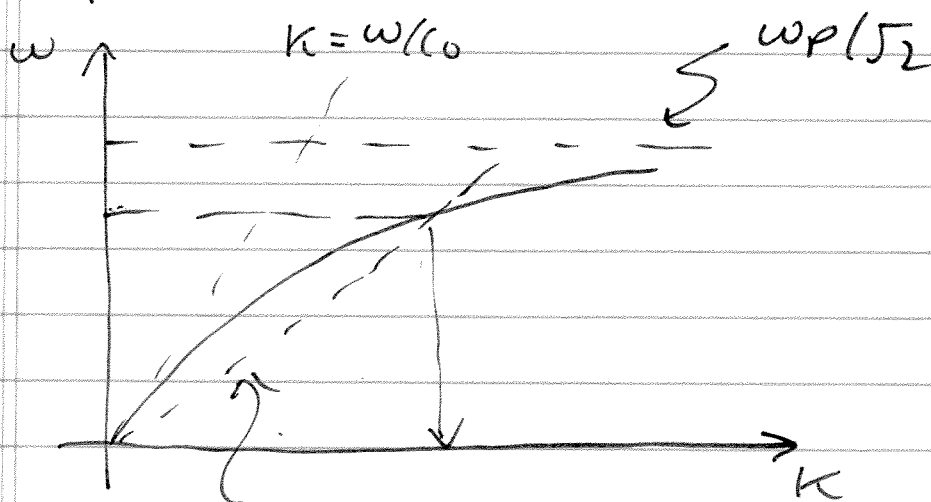
~ excite SPs in films by coupling through a prism

Example: medium ② = air



$$k_{zc} = k n_g \sin \theta$$

$$= \frac{\omega n_g}{c_0} \sin \theta$$



$k = \frac{\omega n_g}{c_0} \sin \theta$ ← tuning the angle allows us to match k 's at different ω s